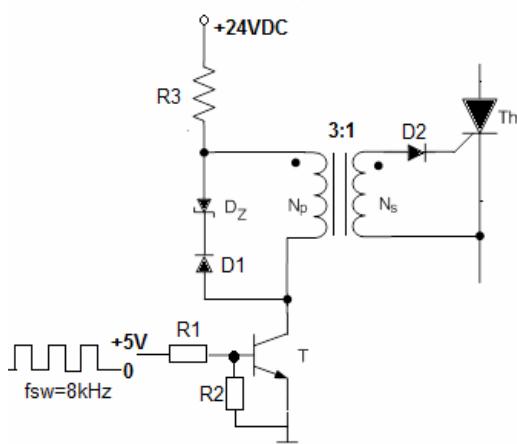


1.ZADATAK: Monofazni AC/AC pretvarač sa anti-paralelnom spregom služi za regulaciju snage otpornog potrošača koji se napaja iz mreže $400V \pm 10\%$, $50Hz$. Na raspolaganju su: tiristorski moduli SKKT460 čiji su podaci dati u Tabeli 1 i hladnjaci P16/200 sa ventilatorom SKF16B čije su karakteristike date u prilogu.
(a)Koliku minimalnu a koliku maksimalnu trajnu prividnu snagu je moguće ostvariti ovim pretvaračem, ako se usvoji da je maksimalno dozvoljena temperatura silicijuma $100^{\circ}C$, a temperatura okoline se menja u opsegu $-25^{\circ}C...+40^{\circ}C$? Koliki je opseg promene temperature hladnjaka pri ovim uslovima?
(b) Dimenzionisati zaštitno kolo „di/dt“ za tiristore.



(c)Dimenzionisati pobudno kolo tiristora prikazano na slici (R_1 , R_2 , R_3 , V_z) , uz pretpostavku da je u kolu gejta tiristora potrebno ostvariti struju od $1.5A$ pri naponu gejt-katoda od $3V$.

NAPOMENE:

Usvojiti da je pad napona na diodama $0.6V$, napon $V_{bes}=0.75V$, napon $V_{ces}=0.2V$, pojačanje tranzistora $hfe=400$. Induktivnost magnećenja impulsnog transformatora je $100mH$, dok je njegova rasipna induktivnost zanemarljiva.

2. ZADATAK:

Potrebito je nacrtati električnu šemu i projektovati AC/DC električni neizolovani pretvarač napona za koji su dati ulazni podaci za projektovanje:

- Nominalni ulazni napon $3x380V \pm 10\%$, $50Hz$
- Izlazni napon $220VDC$
- Izlazna snaga $2.2kW$
- Talasnost struje prigušnice $\leq 20\%$
- Talasnost izlaznog napona $\leq 0.5\%$
- Radna učestanost $50kHz$

-Dimenzionisati prekidačke elemente prema struci i naponu (prema MAX naponu koji moraju izdržati i prema srednjoj vrednosti struje)

-Zanemariti padove napona i komutacione gubitke na prekidačkim elementima, kao i unutrašnje otpornosti pasivnih elemenata.Smatrati da je opterećenje na izlazu približno konstantno

3. ZADATAK: Neizolovani DC/DC pretvarač (naponski podizač) snage $300W$ radi na konstantnoj učestanosti $100kHz$. Ulagani napon iznosi $24V$. Smatrati da je kapacitivnost izlaznog kondenzatora dovoljno velika i zanemariti talasnost izlaznog napona. Pretvarač radi u kontinualnom režimu. Prekidačke elemente u pretvaraču smatrati idealnim.Vremenski interval provođenja diode je $5\mu s$. (a)Odrediti srednju vrednost struje diode, (b) Dimenzionisati prigušnicu L ako se zahteva da talasnost struje ("peak-peak") kroz nju bude manja od 5% , (c) Odrediti minimalnu i maksimalnu vrednost struje prigušnice.

4.ZADATAK:

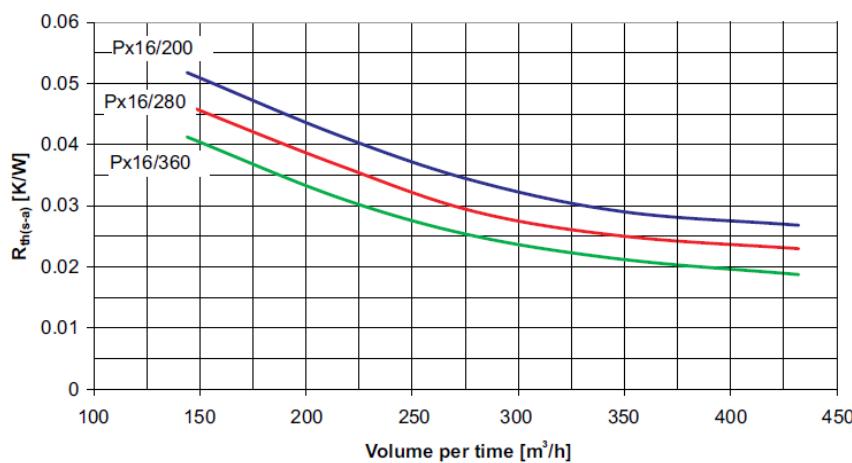
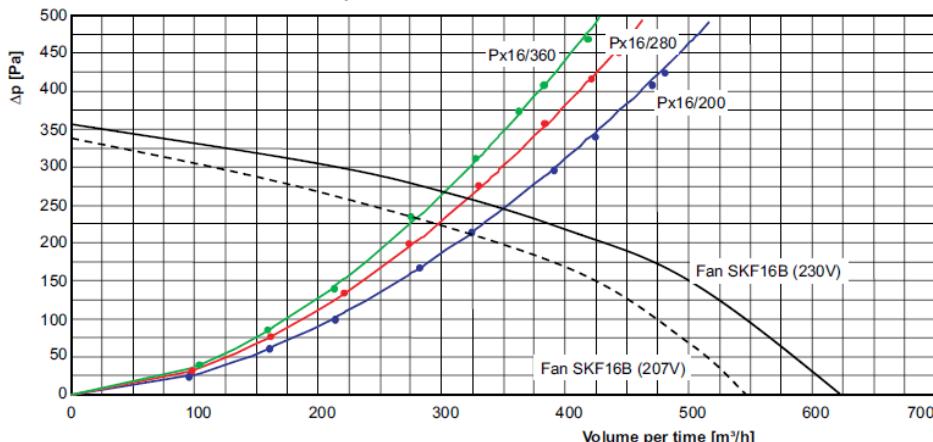
U kolu u zadatuču 3 potrebno je LEM strujnim modulom meriti trenutnu vrednost struje prekidačkog tranzistora na osciloskopu. Na raspolaganju su LEM strujni senzori prenosnog odnosa $1:5000$, napona napajanja $\pm 15V DC$, ali različitih propusnih opsega $1MHz$, $10MHz$, $50MHz$ i $100MHz$ i opseg struja $0-5A$, $10A$, $25A$, $50A$, $100A$. Povraćeno nanelektrisanje diode kod isključenja je $Q_{rr} = 1\mu C$. Vreme oporavka diode je $t_{rr}=50ns$. Odabrati potreban LEM senzor, nacrtati šemu merenja struje i dimenzionisati merni otpornik na izlazu LEM modula tako da se na njemu obezbedi naponski signal $0-5VDC$ koji se vodi na ulaz osciloskopa radi merenja. Vršnu vrednost struje diode (tzv.”strujni pik”) računati prema formuli $I_{RM} \approx 2Q_{rr}/t_{rr}$.

PRILOG ZA ZADATAK 01:

Tabela 1-Karakteristike tiristorskog modula SKKT460

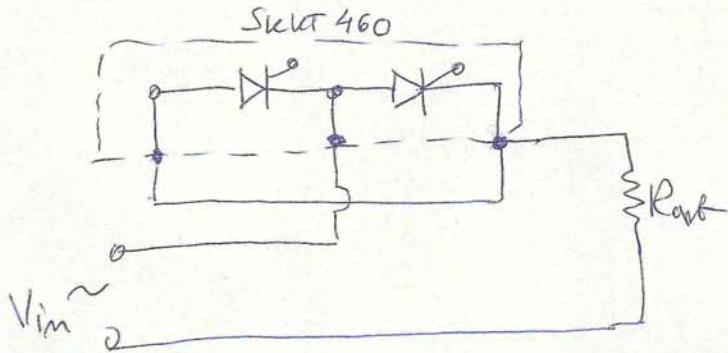
Symbol	Conditions	Values	Units
I_{TAV}	sin. 180; $T_c = 85$ (100) °C;	460 (335)	A
I_{TSM}	$T_{vj} = 25$ °C; 10 ms	18000	A
	$T_{vj} = 130$ °C; 10 ms	15500	A
i^t	$T_{vj} = 25$ °C; 8,3 .. 10 ms	1620000	A²s
	$T_{vj} = 130$ °C; 8,3 ... 10 ms	1200000	A²s
V_T	$T_{vj} = 25$ °C; $I_T = 1400$ A	max. 1,6	V
$V_{T(TO)}$	$T_{vj} = 130$ °C	max. 0,88	V
r_T	$T_{vj} = 130$ °C	max. 0,45	mΩ
I_{DD}, I_{RD}	$T_{vj} = 130$ °C; $V_{RD} = V_{RRM}$; $V_{DD} = V_{DRM}$	max. 240	mA
t_{gd}	$T_{vj} = 25$ °C; $I_G = 1$ A; $dI_G/dt = 1$ A/μs	1	μs
t_{gr}	$V_D = 0,67 * V_{DRM}$	2	μs
$(di/dt)_{cr}$	$T_{vj} = 130$ °C	max. 250	A/μs
$(dv/dt)_{cr}$	$T_{vj} = 130$ °C	max. 1000	V/μs
t_q	$T_{vj} = 130$ °C ,	100 .. 200	μs
I_H	$T_{vj} = 25$ °C; typ. / max.	150 / 500	mA
I_L	$T_{vj} = 25$ °C; $R_G = 33 \Omega$; typ. / max.	300 / 2000	mA
V_{GT}	$T_{vj} = 25$ °C; d.c.	min. 3	V
I_{GT}	$T_{vj} = 25$ °C; d.c.	min. 200	mA
V_{GD}	$T_{vj} = 130$ °C; d.c.	max. 0,25	V
I_{GD}	$T_{vj} = 130$ °C; d.c.	max. 10	mA
$R_{th(j-c)}$	cont.; per thyristor / per module	0,072 / 0,035	K/W
$R_{th(j-c)}$	sin. 180°; per thyristor / per module	0,074 / 0,037	K/W
$R_{th(j-c)}$	rec. 120°; per thyristor / per module	0,078 / 0,039	K/W
$R_{th(c-s)}$	per thyristor / per module	0,02 / 0,01	K/W
T_{vj}		- 40 ... + 130	°C
T_{stg}		- 40 ... + 125	°C

Karakteristike hladnjaka i ventilatora
Pressure drop characteristic for Px16/200 ; Px16/280 ; Px16/360



(1)

12A250



$$V_{in} = 400V \pm 10\%$$

50Hz

$$\begin{array}{c}
 T_j \xrightarrow{P_{tot}} \\
 | \\
 R_{th(j-c)_e} = \frac{R_{th(j-c)}}{2} \\
 | \\
 T_c \xrightarrow{R_{th(c-s)_e} = \frac{R_{th(c-s)}}{2}} \\
 | \\
 T_s \xrightarrow{R_{th(s-a)_e}} \\
 | \\
 T_a
 \end{array}
 \quad
 \begin{array}{l}
 P_{tot} = \frac{T_j - T_a}{\varepsilon R_{th}} \\
 P_{tot} = \frac{T_j - T_a}{R_{th(j-c)_e} + R_{th(c-s)_e} + R_{th(s-a)_e}} \\
 R_{th(j-c)_e} = \frac{9074}{2} = 0,037 \frac{K}{W} \\
 R_{th(c-s)_e} = \frac{0,02}{2} = 0,01 \frac{K}{W} \\
 R_{th(s-a)} = ?
 \end{array}$$

zu $H_{max} = P16/200 \text{ bei } 207V_n \rightarrow \text{proton } 325 \frac{m^3}{h}$

$$zu 325 \frac{m^3}{h} \rightarrow R_{th(s-a)} = 0,03 \frac{K}{W}$$

$$P_{tot_1} = \frac{100 - (-25)}{0,037 + 0,01 + 0,03} = 1623,3 W = 1,62 kW$$

$$P_{tot_2} = \frac{100 - 40}{0,037 + 0,01 + 0,03} = 779,2 W \rightarrow 0,78 kW$$

$$\begin{aligned}
 & \text{zu zweiter } P_{tot_1}^{(1)} = V_{TO} \frac{I_{m1}}{\pi} + r_d \frac{I_{m1}^2}{4} = \frac{P_{tot_1}}{2} = 811,6 W \\
 & \text{zu zweiter } P_{tot_2}^{(1)} = V_{TO} \frac{I_{m1}}{\pi} + r_d \frac{I_{m1}^2}{4} = \frac{P_{tot_2}}{2} = 390,6 W
 \end{aligned}$$

(2)

$$P_{\text{tot},1}^{(1)} = V_{T0} \cdot \frac{\bar{I}_{m1}}{\pi} + r_d \frac{\bar{I}_{m1}^2}{4} \cdot \frac{1}{r_d}$$

$$\frac{4}{r_d} \cdot P_{\text{tot},1}^{(1)} = \frac{4V_{T0}\bar{I}_{m1}}{\pi r_d} + \bar{I}_{m1}^2$$

17. Masse 1:

$$V_{T0} = 0,9$$

$$r_d = 0,45 \mu\Omega$$

$$P_{\text{tot},1}^{(1)} = 811,65 \text{ W}$$

$$\bar{I}_{m1} = - \frac{2V_{T0}}{\pi r_d} \pm \sqrt{\frac{4V_{T0}^2}{(\pi r_d)^2} + \frac{16 P_{\text{tot},1}^{(1)}}{4r_d}}$$

$$\bar{I}_{m1} = - \frac{2 \cdot 0,9}{\pi \cdot 0,45} \cdot 10^3 \pm \sqrt{\frac{4 \cdot (0,9)^2}{(\pi \cdot 0,45)^2} \cdot 10^6 + \frac{16 \cdot 811,65}{4 \cdot 0,45} \cdot 10^3}$$

$$= - 1,274 \cdot 10^3 \pm \sqrt{1,6228 \cdot 10^6 + 7,214 \cdot 10^6}$$

$$= - 1,274 \cdot 10^3 \pm 2,973 \cdot 10^3 \Rightarrow \bar{I}_{m1} = 16994$$

Effektivem meaner für die optische:

$$= \underline{17004}$$

$$I_{\text{eff},\text{opt},1} = \frac{1700}{\sqrt{2}} = \underline{\underline{1200 \text{ A}}}$$

$$I_{TAV} = \frac{\bar{I}_{m1}}{\pi} = 540 \text{ A} > \boxed{\begin{aligned} I_{TAV,\text{DZV}} &= 460 \text{ A NA} + 80^\circ\text{C} \\ &= 335 \text{ A NA} + 100^\circ\text{C} \end{aligned}} \quad \text{Masse 1 zu Masse 2} \\ \text{DZV: Verlustwärme}$$

$$S_{\text{opt}} = \frac{\pi \cdot 335 \text{ A} \cdot 440 \text{ V}}{\sqrt{2}} = \underline{\underline{327,2 \text{ kW}}}$$

$$\underset{I_{\text{eff},\text{opt},1} = 1200 \text{ A}}{P_{\text{tot},1}^*} = V_{T0} \cdot \frac{\bar{I}_{m1}}{\pi} + r_d \frac{\bar{I}_{m1}^2}{4} = 0,9 \cdot 335 \cdot \pi + 0,45 \mu\Omega \cdot \left(\frac{335 \pi}{4} \right)^2 = 1071 \text{ W}$$

$$T_{\text{A}} = R_{th,s-a} \cdot P_{\text{tot},1}^* + T_{\text{A}1} = 0,03 \cdot 1073 + (-25^\circ\text{C}) = 7,13^\circ\text{C}$$

$$* \quad \text{if } I_{TAV} = 460 \text{ A} \quad \bar{I}_{m1} = \pi \cdot 460 = 1450 \text{ A} \Rightarrow I_{\text{eff}} = \frac{\bar{I}_{m1}}{\sqrt{2}} = 1024 \text{ A}$$

$$I_{\text{eff},\text{opt}} = 1024 \text{ A} \rightarrow S_{\text{opt}} = 1024 \cdot 440 = 450 \text{ kW}$$

$$* \quad \text{if } I_{TAV} = 540 \text{ A} \quad \bar{I}_{m1} = \pi \cdot 540 = 1696 \text{ A} \Rightarrow I_{\text{eff}} = \frac{\bar{I}_{m1}}{\sqrt{2}} = 1200 \text{ A}$$

$$I_{\text{eff},\text{opt}} = 1200 \text{ A} \rightarrow S_{\text{opt}} = 1200 \cdot 440 = 530 \text{ kW}$$

(3)

$$P_{tot_2}^{(1)} = \frac{P_{tot_2}}{2} = \frac{780}{2} = 390W$$

$$P_{tot_2}^{(1)} = V_{to} \frac{\bar{I}_{m2}}{\pi} + r_d \frac{\bar{I}_{m2}^2}{4} \quad \bar{I}_{m2} = -\frac{2V_{to}}{\pi r_d} \pm \sqrt{\frac{4V_{to}^2}{(\pi r_d)^2} + \frac{16 P_{tot_2}^{(1)}}{4 r_d}}$$

$$\bar{I}_{m2} = -\frac{2 \cdot 0,9}{\pi \cdot 0,45} \cdot 10^3 \pm \sqrt{\frac{4 \cdot (0,9)^2}{(\pi \cdot 0,45)^2} \cdot 10^6 + \frac{16 \cdot 390}{4 \cdot 0,45} \cdot 10^3}$$

$$\begin{aligned} \bar{I}_{m2} &= -1,274 \cdot 10^3 \pm \sqrt{1,6228 \cdot 10^6 + 3,466 \cdot 10^6} \\ &= -1,274 \cdot 10^3 \pm 2,255 \cdot 10^3 \end{aligned}$$

$$\bar{I}_{m2} = 0,982 \text{ A.} \approx 982 \text{ A}$$

$$I_{eff, opt_2} = \frac{\bar{I}_{m2}}{\sqrt{2}} = \frac{982}{\sqrt{2}} = 696 \text{ A.}$$

$$I_{DN} = \frac{\bar{I}_{m2}}{\pi} = \underline{312 \text{ A}}$$

$$S_{opt} = 696 \text{ A} \cdot 440 \text{ V} \approx 306,2 \text{ kW}$$

~~Temperatur~~ Temperatur in einer Spule

$$\begin{aligned} T_{S2} &= R_{th}(s-a) \cdot P_{tot_2} + T_{a2} \\ &= 0,034 \text{ W} \cdot 780 \text{ W} + 40^\circ \text{C} \\ &= 63,4^\circ \text{C.} \end{aligned}$$

$$23,69^\circ \text{C} \leq T_S \leq 63,4^\circ \text{C}$$

$$S_{max} = P_{max} = 320 \text{ kW} \quad \begin{array}{l} \text{MAX. SWATT} \\ \text{wurde} \\ \text{erreicht} \end{array}$$

(7)

b)

$$\left| \frac{di_T}{dt} \right|_{t=0} = \frac{U_m}{L_u} \leq 250 \frac{A}{\mu s} \Rightarrow L_u \geq \frac{U_m}{250 \frac{A}{\mu s}}$$

$$U_m = 400 \cdot 1,1 \cdot \sqrt{2} = 620,4 V$$

$$L_u \geq \frac{620,4}{250 \frac{A}{\mu s}} = 2,48 \mu H \rightarrow \underline{\underline{L_u = 3 \mu H}}$$

~~zu~~ $L_u = 3 \mu H \rightarrow \frac{di_T}{dt} = \frac{U_m}{L_u} = \frac{620,4 V}{3 \mu H} = 206,6 \frac{A}{\mu s} < 250 \frac{A}{\mu s}$

c)

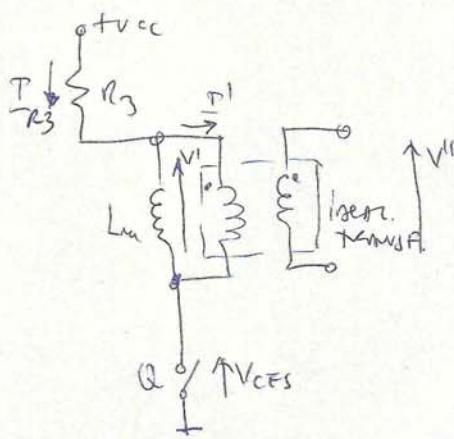
$$T_{SW} = \frac{1}{f} = \frac{1}{800 Hz} = 1,25 \mu s$$

$$V^{II} = V_{GE} + V_D = 3 + 0,6 = 3,6 V$$

$$V^I = \frac{N^I}{N^{II}} \cdot V^{II} = m \cdot V^{II} = 3 \cdot 3,6 = 10,8 V$$

$$I^{II} = I_g = 1,5 A \quad I^I = \frac{I^{II}}{3} = \frac{1,5}{3} = 0,5 A$$

$$t_{on} = t_{off} \quad t_{on} + t_{off} = 2 \cdot 62,5 \mu s \Rightarrow t_{on} = t_{off} = \frac{1}{2} T = 62,5 \mu s$$



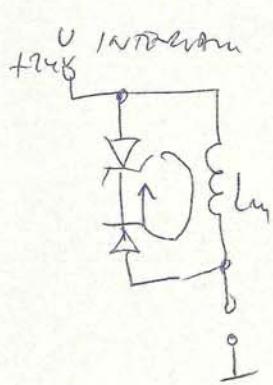
$$V_{CC} = R_3 I^I + V^I + V_{CES}$$

$$R_3 = \frac{V_{CC} - V^I - V_{CES}}{I^I} = \frac{24 - 10,8 - 0,2}{0,5} = 26 \Omega$$

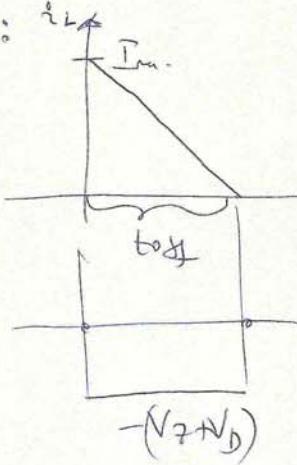
$$I_{eff} = \frac{I^I}{\sqrt{2}} = \frac{0,5}{\sqrt{2}} = 0,35 A$$

$$P_{R3} = R_3 I_{eff}^2 = 26 \cdot 0,35^2 = 3,185 W$$

$$R_3 = 22 \Omega / 5W$$



$$t_{off} : t_{on}$$



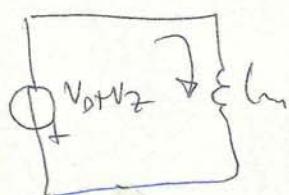
$$L_m \Delta i = V_f t_m$$

$$\Delta i = I_m$$

$$I_m = \frac{V_f t_m}{L_m}$$

$$I_m = \frac{10,8 \cdot 67,5 \mu s}{100 \cdot 10^{-3}}$$

$$I_m = 6,2 \text{ mA.}$$



$$L_m \cdot \Delta i = (V_D + V_Z) t_{off}$$

$$t_{off} \leq 67,5 \mu s.$$

$$t_{off} = \frac{L_m \Delta i}{V_D + V_Z} \leq 67,5 \mu s.$$

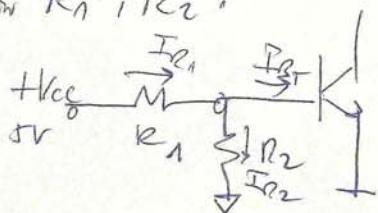
$$V_D + V_Z > \frac{L_m \Delta i}{67,5 \mu s} = 11,12 \text{ V} \quad V_D = 0,6$$

$$V_Z = 11,7 - 0,6 = 10,5 \text{ V} \rightarrow V_Z^* = 11 \text{ V}$$

$$\Phi_{D2} = 11 \text{ V} \cdot 6,7 \text{ mA} = 0,0737 \rightarrow 11 \text{ V} / 0,125 \text{ W}$$

$$V_{BE2} \text{ max } R_2 = 10 \Omega$$

Praktisch R1 | R2:



$$I_{R2} = \frac{V_{BE2}}{R_2} = \frac{0,75}{10 \cdot 10^3} = 0,075 \text{ mA}$$

$$I_C' = I_B' = 0,5 \text{ A}$$

$$I_{BT} = \frac{0,5}{100} \Rightarrow I_{BT} = 1,25 \text{ mA}$$

$$I_{R1} = I_{BT} + I_{R2} = 0,075 \text{ mA} + 1,25 \text{ mA} = 1,325 \text{ mA}$$

$$V_{CC} = R_1 I_{R1} + V_{BE2} \Rightarrow R_1 = \frac{V_{CC} - V_{BE2}}{I_{R1}} = \frac{11 - 0,75}{1,325} \cdot 10^3$$

$$R_1 = 3,21 \text{ k}\Omega \xrightarrow{\text{versim}} 3,3 \text{ k}\Omega$$

(6)

$$P_{R1} = R_1 I_{R1}^2 = 3,3 \cdot 10^3 \cdot 1,375^2 \cdot 10^{-6} = 6 \text{ mW}$$

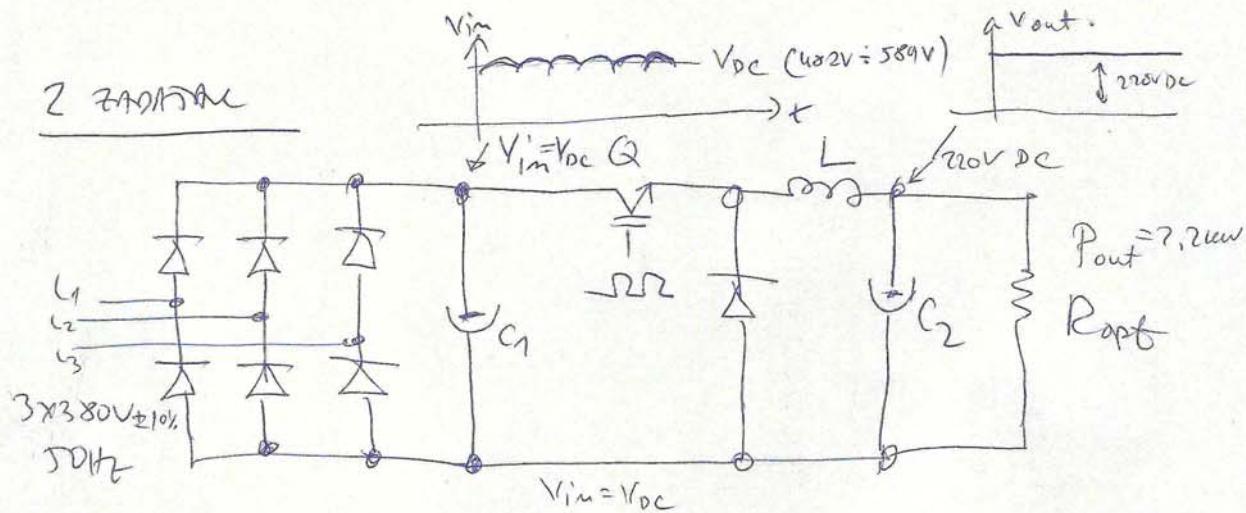
$$P_{R2} = R_2 I_{R2}^2 = 10 \cdot 10^3 \cdot 0,075^2 \cdot 10^{-6}$$

$$P_{R2} = 0,75 \text{ mW}$$

$$R_1 = 3,3 \text{ k}\Omega / 10 \text{ mW}$$

$$R_2 = 10 \text{ m}\Omega / 1 \text{ mW}$$

$$R_3 = 27 \text{ }\mu\Omega / 5 \text{ mW}$$



$$\frac{\Delta V_{in}}{V_{in}} = \frac{\Delta V_{in}}{V_{DC}} = 2 \cdot \frac{1}{12 f R_{load} C - 1} \Rightarrow 12 f R_{load} C - 1 = \frac{2}{\frac{\Delta V_{in}}{V_{DC}}}$$

$$C_1 = \left(1 + \frac{2 V_{DC}}{\Delta V_{in}} \right) / 12 f R_{load}$$

$$C_1 = \frac{1 + \frac{2 V_{DC}}{\Delta V_{in}}}{12 f R_{load}} = \frac{1 + \frac{2 V_{DC}}{\Delta V_{in}} \cdot \frac{V_{DC}}{I_{DC}}}{12 f \cdot \frac{V_{DC}}{I_{DC}}} = \frac{1 + \frac{2}{\frac{\Delta V_{in}}{V_{DC}}}}{12 f \cdot \frac{V_{DC}}{I_{DC}}} \xrightarrow[5\%]{\frac{\Delta V_{in}}{V_{DC}} \approx 0,05}$$

$$C_1 \geq \frac{1 + \frac{2}{0,05}}{12 \cdot 50 \cdot \frac{500}{4,4}} = \frac{41}{68182} = 601,33 \mu\text{F}$$

Minimales C = 680 μF. $V_{in} = V_{DC} \approx U_{eff, max} \cdot \sqrt{2}$

$$V_{in, min} = V_{DC, min} = (380 - 38) \sqrt{2} = 482,12 \text{ V}$$

$$V_{in, max} = V_{DC, max} = (380 + 38) \sqrt{2} = 589,38 \text{ V}$$

$\frac{482,12}{589,38} (V_{in} = V_{DC}) \leq 589,38 \text{ V}$

$$482,2V \leq V_{in} \leq 589,38V \quad (7)$$

$$I_{LSE} = I_{out} = \frac{220V}{22\Omega} = 10A$$

$$R_{opt} = \frac{V_{out}^2}{P} = \frac{220^2}{2200} = 22\Omega$$

$$\Delta i_L = \frac{\Delta i_L}{I_{out} \cdot 100} = \frac{10 \cdot 20}{100} = 2A$$

$$L \geq \frac{(V_{imax} - V_{out}) \delta_{min}}{f_{sw} \cdot \Delta i_L}$$

$$\delta_{min} \cdot V_{imax} = 220$$

$$\delta_{min} = \frac{220}{589,38} = 0,373$$

$$\delta_{max} \cdot V_{imax} = 220$$

$$\delta_{max} = \frac{220}{482,2} = 0,456$$

$$L \geq \frac{589,38 - 220}{50 \cdot 10^3 \cdot 2} = 3,7mH \rightarrow \underline{4mH}$$

$$\underline{L^* = 4mH}$$

Vomta se in minimalni frekvenca (482,2V) pri $L^* = 4mH$

$$\Delta i_L = \frac{V_{imax} - V_{out}}{L^*} \cdot \frac{\delta_{max}}{f_{sw}} = \frac{(482,2 - 220) \cdot 0,456}{4 \cdot 10^{-3} \cdot 50^2 \cdot 10^6} = 0,59A$$

$$\therefore \Delta i_L < 2A$$

$$C_2 = \frac{1 - \delta_{min}}{8 \cdot L^* \cdot f_{sw}^2 \left(\frac{V_{out}}{V_{out}} \right)} = \frac{1 - 0,373}{8 \cdot 4 \cdot 10^{-3} \cdot 50^2 \cdot 10^6 \cdot 0,005} = \frac{0,627}{400000}$$

$0,5\% \Rightarrow 0,005$

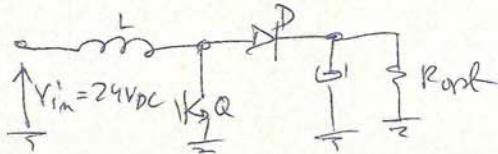
$$C_2 = 1,567 \mu F \leftrightarrow \text{mentno } C_2 = \underline{2,2 \mu F} \quad (\text{curenje } 2e5041Hz)$$

$$\omega_{net} = \frac{1}{\sqrt{L^* C_2^*}} = \frac{1}{\sqrt{4 \cdot 10^{-3} \cdot 2,2 \cdot 10^{-6}}} = 10660 \text{ rad/s}$$

$$f_{net} = \frac{\omega_{net}}{2\pi} = 1,697 \text{ kHz} \ll f_{sw} \text{ je}$$

Dioda mora da popređe maksimalno 0,220V \rightarrow max broj matici 400V
 neka greje uverljivo gase (MAX) $(1 - \delta_{min}) \cdot I_{out} = (1 - 0,373) \cdot 10A = 6,27A$
 usisano diodi D: $10A/400V > 2A$ tada je $I_{TSE} = 0,456 \cdot 10 = 4,56A \rightarrow 10A$
 da je maksimalni tok na rednjim 600V \rightarrow maksimalna TJEZ. $10A/1000V$

3. Zählpulse.



$$P_{out} = 300 \text{ W} \quad (8)$$

$$f_{sw} = 100 \text{ kHz} \rightarrow T = 10 \mu\text{s}.$$

$$t_{off} = 5 \mu\text{s} \rightarrow t_{on} = 5 \mu\text{s}$$

$$\delta = \frac{t_{on}}{T} = \frac{1}{2}$$

$$V_{out} = \frac{V_{in}}{1 - \delta} = \frac{V_{in}}{1 - 0,5} = 2 V_{in} = 48 \text{ V DC}$$

$$R_{out} = \frac{48 \text{ V}}{I_{out}} \quad I_{out} = \frac{P_{out}}{V_{out}} = \frac{300}{48} = 6,25 \text{ A}$$

$$R_{out} = \frac{48}{6,25} = 7,68 \Omega$$

a) $I_{Dsr} = I_{out} = 6,25 \text{ A}$

b) $V_{in} \cdot t_{on} = L \Delta i \quad \frac{\Delta i}{I_{in}} \cdot 100 \leq 5 \Rightarrow \Delta i = \frac{5 \cdot I_{in}}{100}$

$$\frac{V_{in} \cdot t_{on}}{L} \leq 0,625 \text{ A}$$

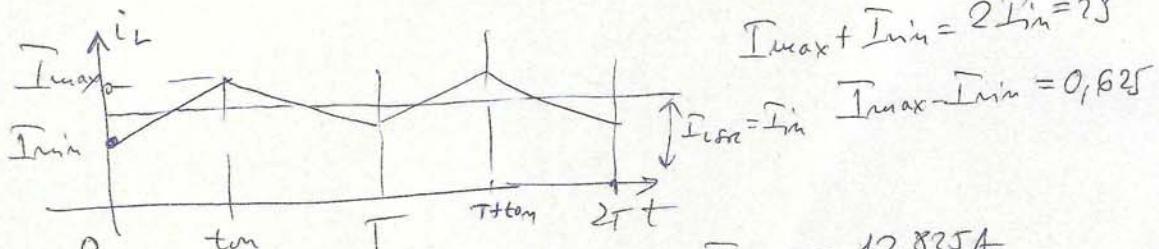
$$I_{in} = \frac{300 \text{ W}}{24 \text{ V}} = 12,5 \text{ A}$$

$$\Delta i = \frac{5 \cdot 12,5}{100} = 0,625 \text{ A}$$

$$L \geq \frac{V_{in} \cdot t_{on}}{0,625 \text{ A}} = \frac{24 \cdot 0,5 \cdot 10 \mu\text{s}}{0,625 \text{ A}}$$

$$L \geq 192 \mu\text{H} \rightarrow \text{Mindestes}$$

$$L = 200 \mu\text{H}$$



$$I_{max} + I_{min} = 2 I_{in} = 25$$

$$I_{max} - I_{min} = 0,625$$

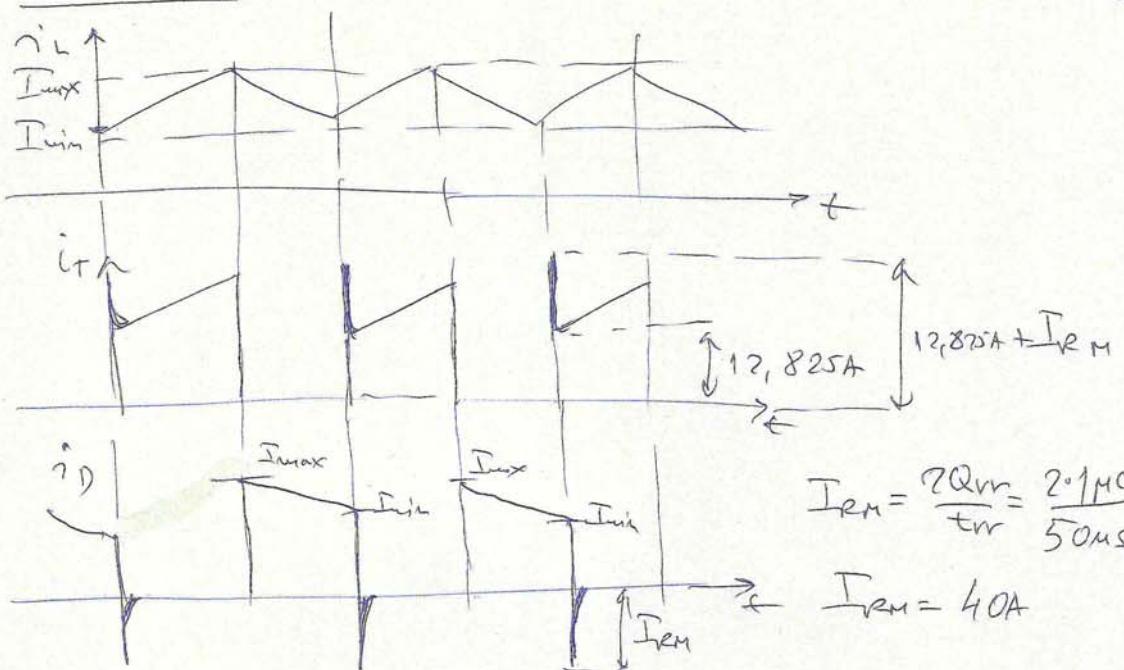
$$2 I_{max} = 25 + 0,625 \Rightarrow I_{max} = 12,825 \text{ A}$$

$$I_{min} = I_{max} - \Delta i = 12,825 - 0,625 = 12,2 \text{ A.}$$

$$\boxed{\begin{aligned} I_{max} &= 12,825 \text{ A} \\ I_{min} &= 12,2 \text{ A} \end{aligned}}$$

4 Zählpunkte:

(9)



$$I_{rm} = \frac{2Q_{rr}}{t_{rr}} = \frac{2 \cdot 1 \text{ mC}}{50 \mu\text{s}}$$

$$I_{rm} = 40 \text{ A}$$

$$I_{\text{MAX PREWINDING-STATE}} = 12,825 \text{ A} + 40 \text{ A} = 13,225 \text{ A} \rightarrow \text{BEMO LEM za 100A}$$

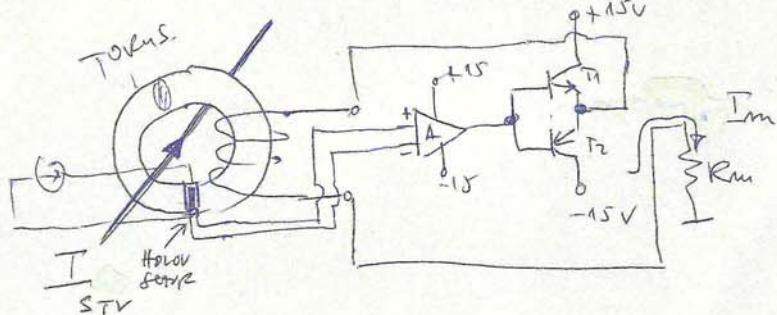
Oben nur da dc $t_{rr} = 50 \mu\text{s}$, $\frac{1}{t_{rr}} \approx 20 \text{ kHz} \rightarrow \text{LEM za 100A}$
resonante
verl. prop.
oder 100MHz

$$R_{mz} \cdot \frac{100 \text{ A}}{5000} = 5 \text{ V} \Rightarrow R_m = 250 \Omega.$$

Symmetrische Kurven werden erwartet $\frac{100 \text{ A}}{5000} = 20 \mu\text{A}$

$$P_{Diss} = R_m I_m^2 = 250 \cdot (0,1 \text{ A})^2 = 0,1 \text{ W} \Rightarrow \text{nichtlineare Messung}$$

$250 \Omega / 0,1 \text{ W}$



U Beogradu 30.01.2018-Predmetni profesor: Dr Željko Despotović, dipl.el.inž.